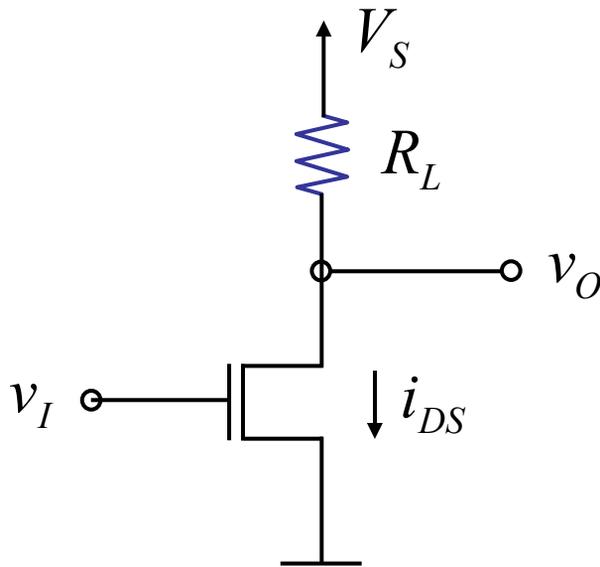


**Amplifiers --  
Small Signal Model**

# Review

## ■ MOSFET amp



## ■ Saturation discipline – operate MOSFET only in saturation region

## ■ Large signal analysis

1. Find  $v_O$  vs  $v_I$  under saturation discipline.
2. Valid  $v_I, v_O$  ranges under saturation discipline.

**Reading: Small signal model -- Chapter 8**

# Large Signal Review

①  $v_O$  vs  $v_I$

$$v_O = V_S - \frac{K}{2} (v_I - 1)^2 R_L$$

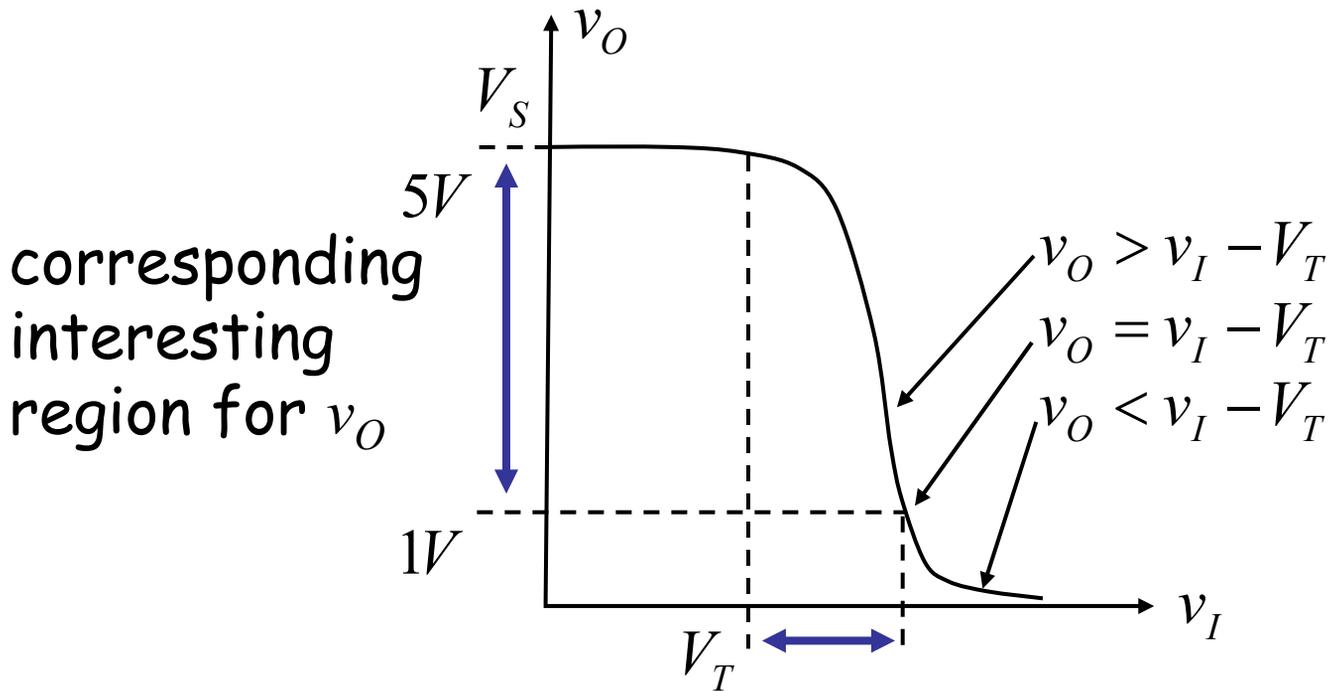
valid for  $v_I \geq V_T$   
and

$$v_O \geq v_I - V_T$$

(same as  $i_{DS} \leq \frac{K}{2} v_O^2$  )

# Large Signal Review

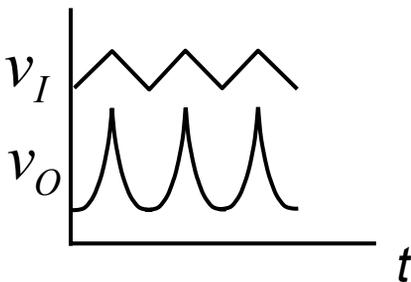
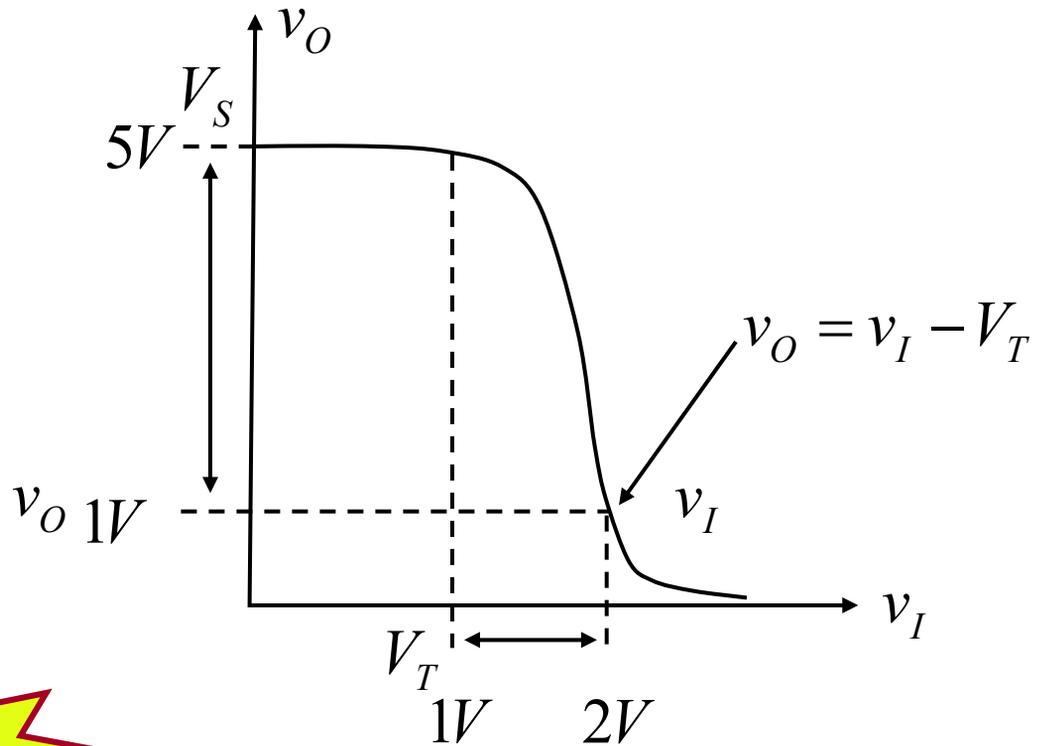
## ② Valid operating ranges



1V 2V

"interesting" region for  $v_I$ . Saturation discipline satisfied.

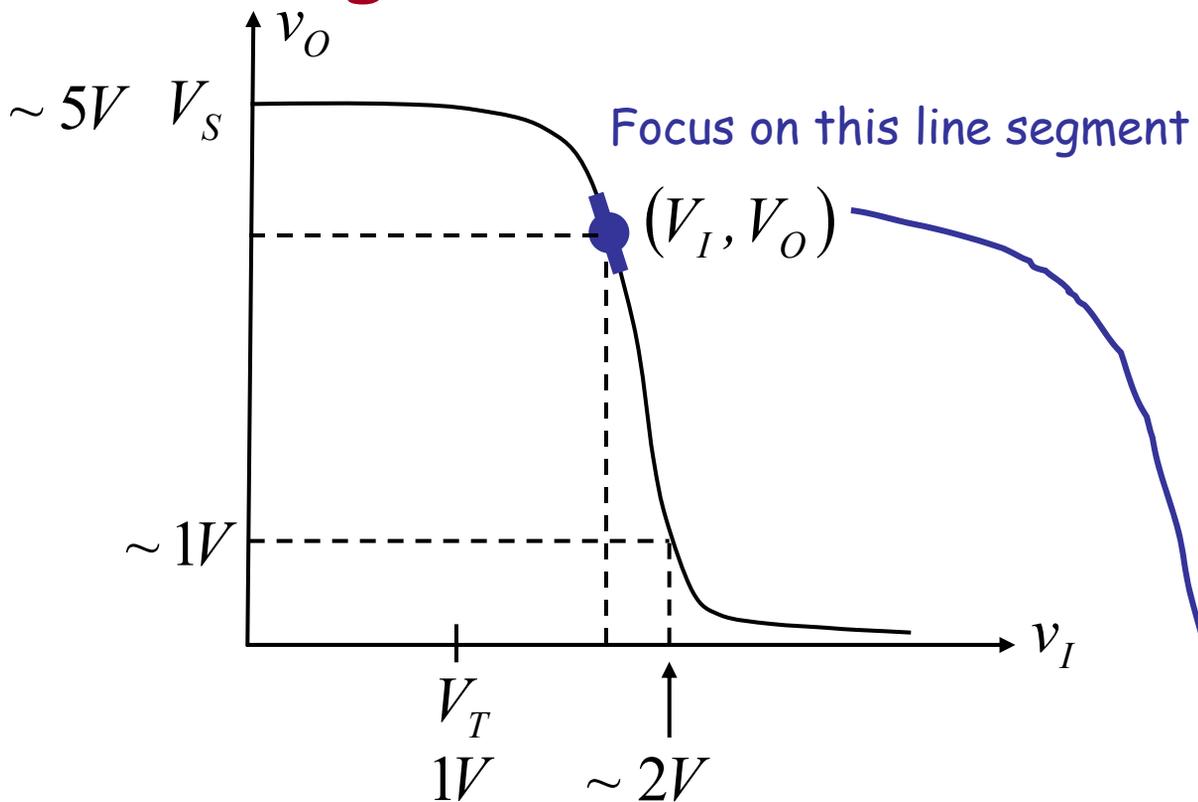
But...



Amplifies alright,  
but distorts

Amp is nonlinear ... ☹️

# Small Signal Model



$$v_O = V_S - \frac{K(v_I - V_T)^2}{2} R_L$$

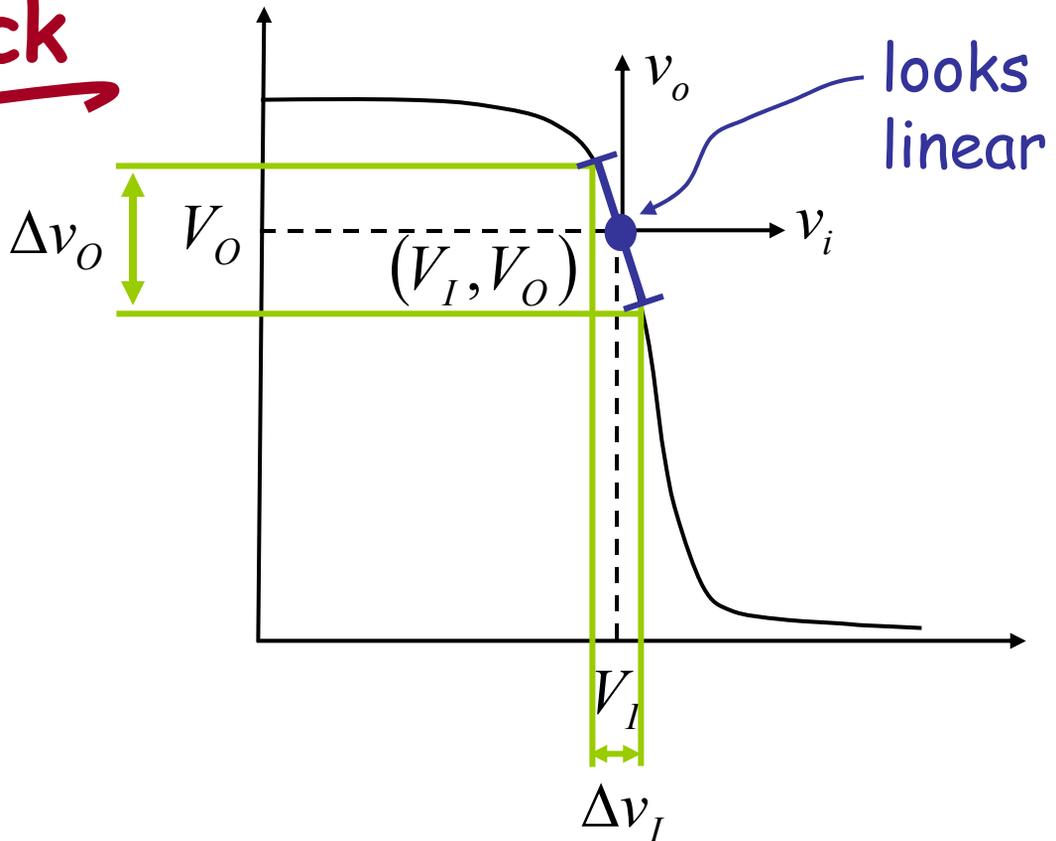
Amp all right, but nonlinear!

Hmmm ... So what about our linear amplifier ???

Insight:

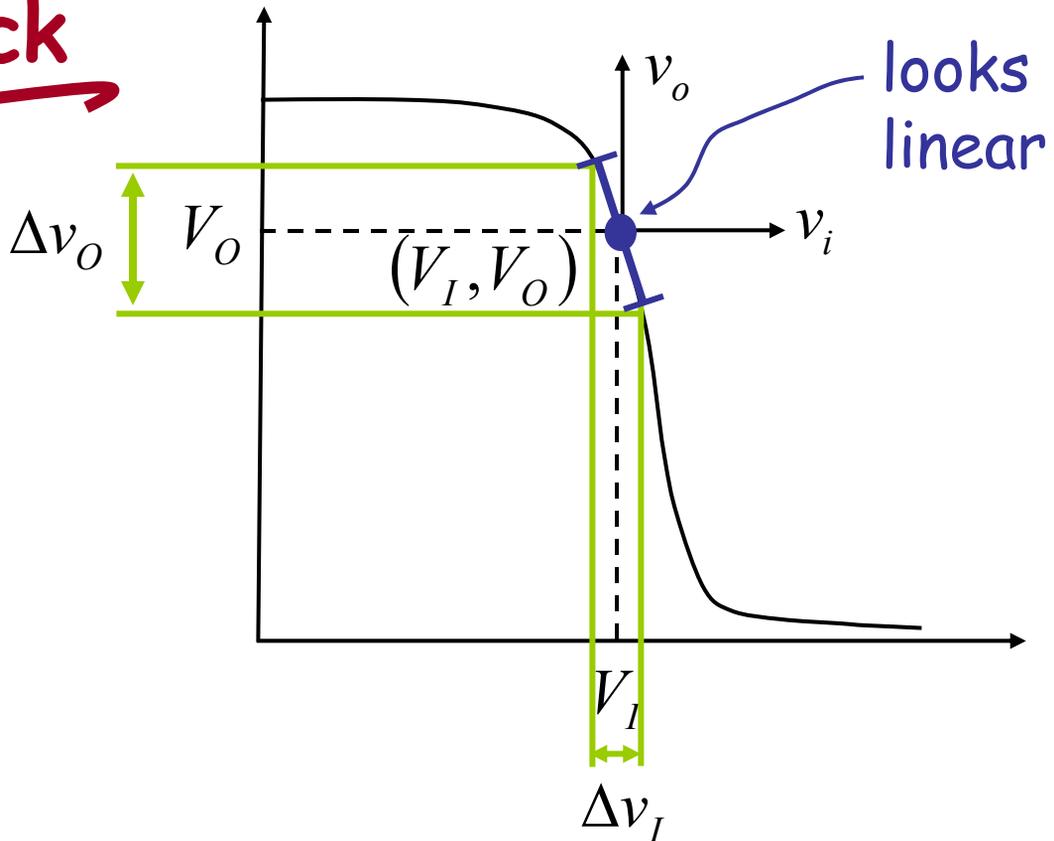
But, observe  $v_I$  vs  $v_O$  about some point  $(V_I, V_O)$  ... looks quite linear!

**Trick**



- ❖ Operate amp at  $V_I, V_O$   
→ DC "bias" (good choice: midpoint of input operating range)
- ❖ Superimpose small signal on top of  $V_I$
- ❖ Response to small signal seems to be approximately linear

# Trick



- ❖ Operate amp at  $V_I, V_O$   
→ DC "bias" (good choice: midpoint of input operating range)
- ❖ Superimpose small signal on top of  $V_I$
- ❖ Response to small signal seems to be approximately linear

Let's look at this in more detail —

I graphically

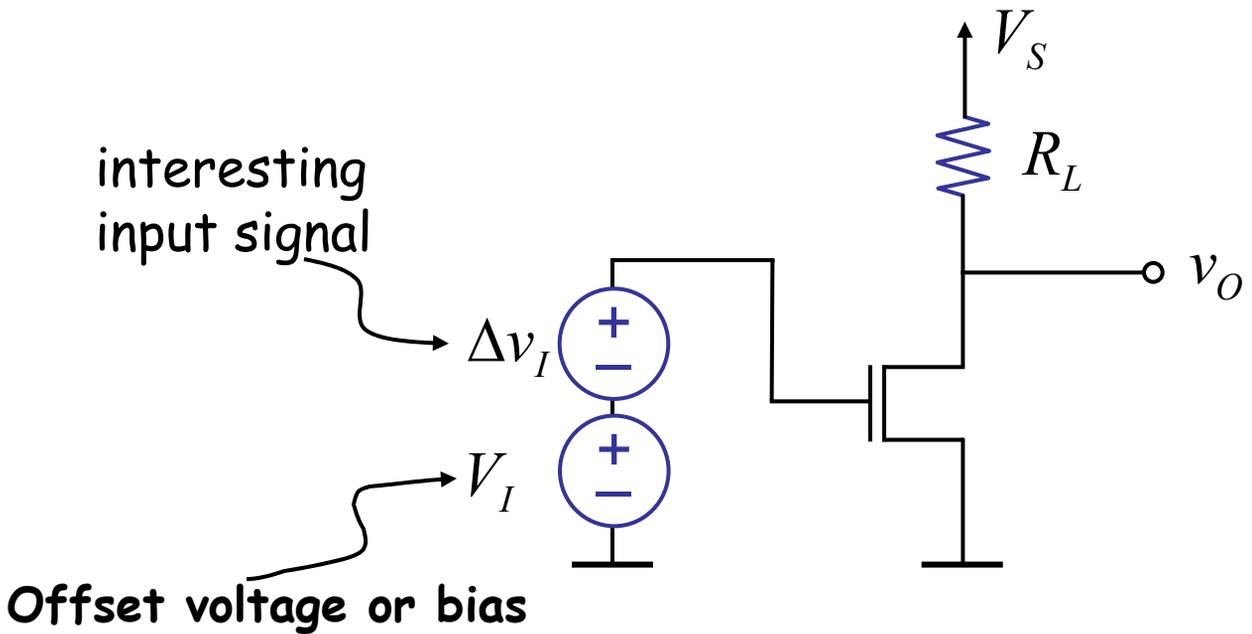
II mathematically

III from a circuit viewpoint

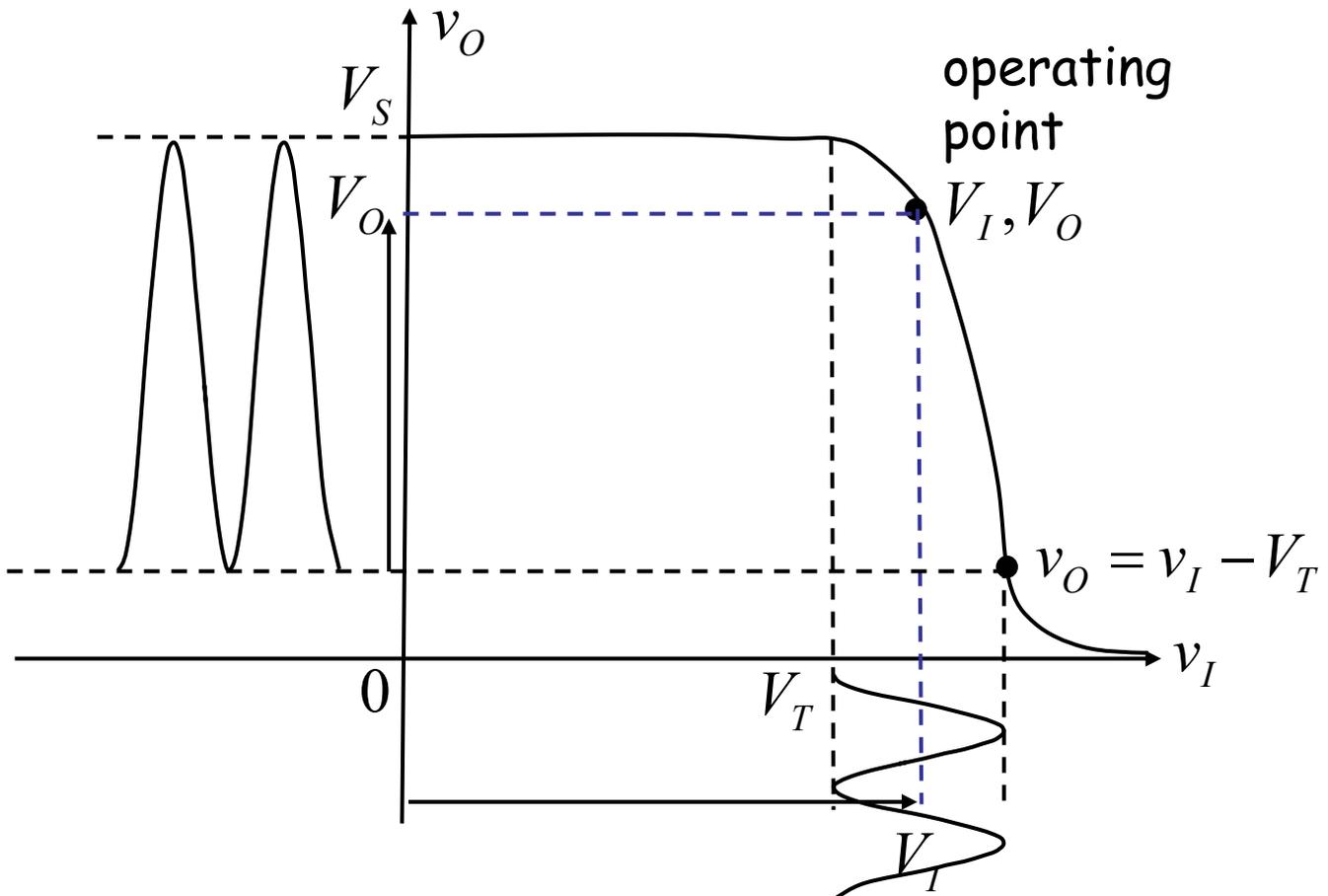
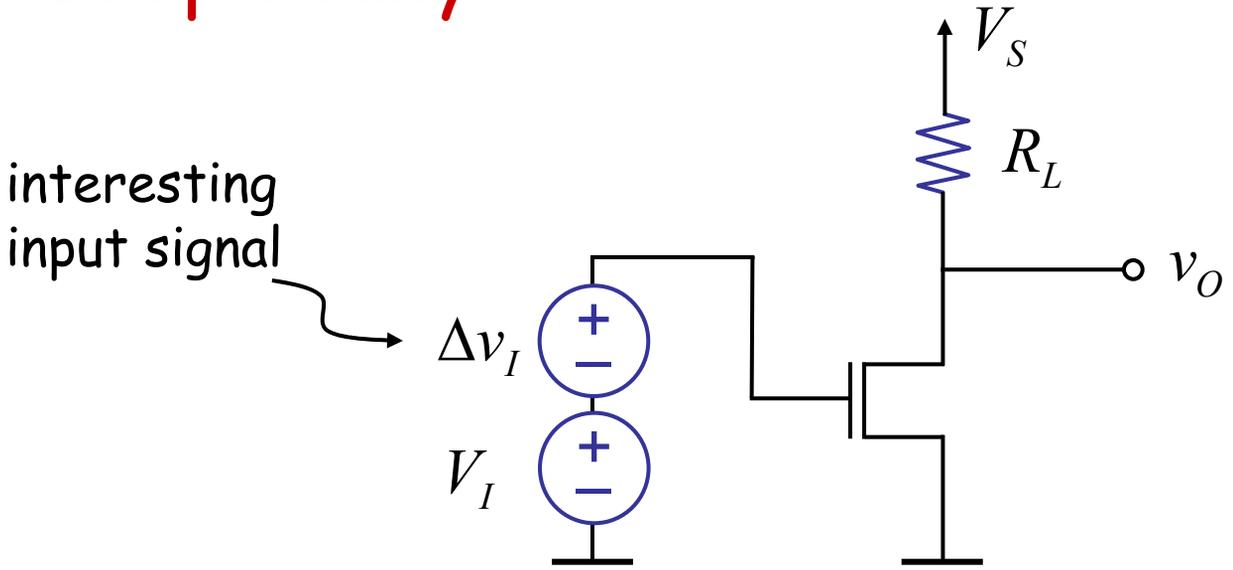
next week

# I Graphically

We use a DC bias  $V_I$  to "boost" interesting input signal above  $V_T$ , and in fact, well above  $V_T$ .



# Graphically



Good choice for operating point:  
midpoint of input operating range

# Small Signal Model

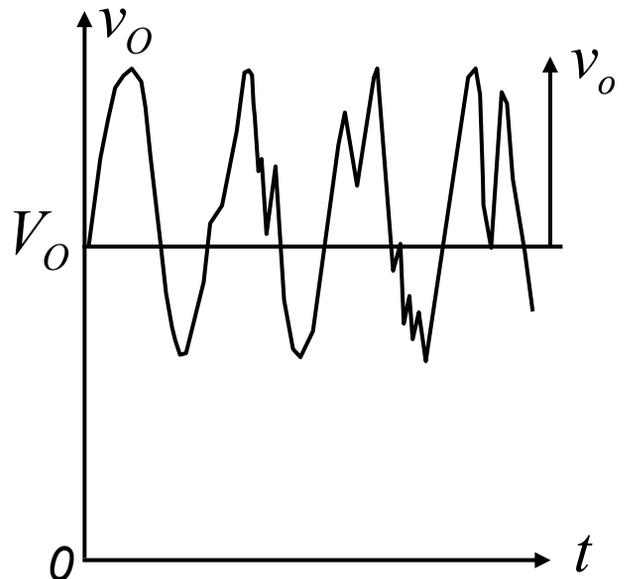
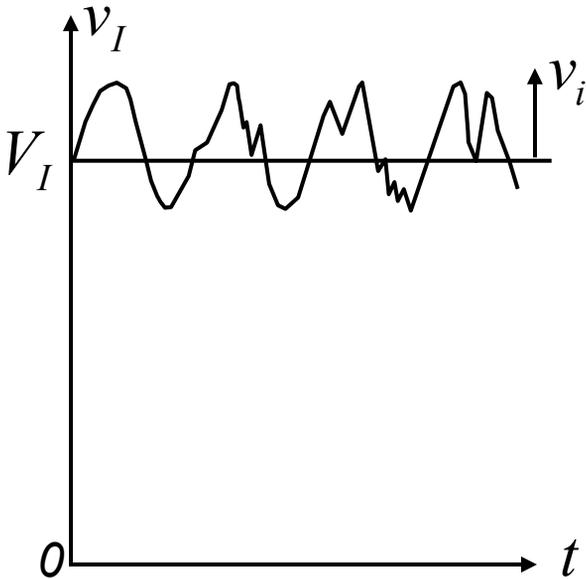
aka incremental model  
aka linearized model

## Notation —

Input:  $v_I = V_I + v_i$   
total variable      DC bias      small signal (like  $\Delta v_I$ )  
bias voltage aka operating point voltage

Output:  $v_O = V_O + v_o$

Graphically,



## II Mathematically

(... watch my fingers)

$$v_o = V_S - \frac{R_L K}{2} (v_I - V_T)^2 \quad \Bigg| \quad V_o = V_S - \frac{R_L K}{2} (V_I - V_T)^2$$

substituting  $v_I = V_I + v_i$   $v_i \ll V_I$

$$v_o = V_S - \frac{R_L K}{2} ([V_I + v_i] - v_T)^2$$

$$= V_S - \frac{R_L K}{2} ([V_I - V_T] + v_i)^2$$

$$= V_S - \frac{R_L K}{2} ([V_I - V_T]^2 + 2[V_I - v_T]v_i + v_i^2)$$

$$V_o + v_o = V_S - \frac{R_L K}{2} (V_I - V_T)^2 - R_L K (V_I - V_T)v_i$$

From  $\star$ ,

$$v_o = - \underbrace{R_L K (V_I - V_T)}_{g_m} v_i \quad \text{related to } V_I$$

# Mathematically

$$v_o = -R_L \underbrace{K (V_I - V_T)}_{g_m} v_i \quad \text{related to } V_I$$

$$v_o = -g_m R_L v_i$$

For a given DC operating point voltage  $V_I$ ,  $V_I - V_T$  is constant. So,

$$v_o = -A v_i$$

  
constant w.r.t.  $v_i$

In other words, our circuit behaves like a linear amplifier for small signals

# Another way

$$v_o = V_S - \frac{R_L K}{2} (v_I - V_T)^2$$

$$v_o = \frac{d}{dv_I} \left[ V_S - \frac{R_L K}{2} (v_I - V_T)^2 \right] \Big|_{v_I = V_I} \cdot v_i$$

slope at  $V_I$

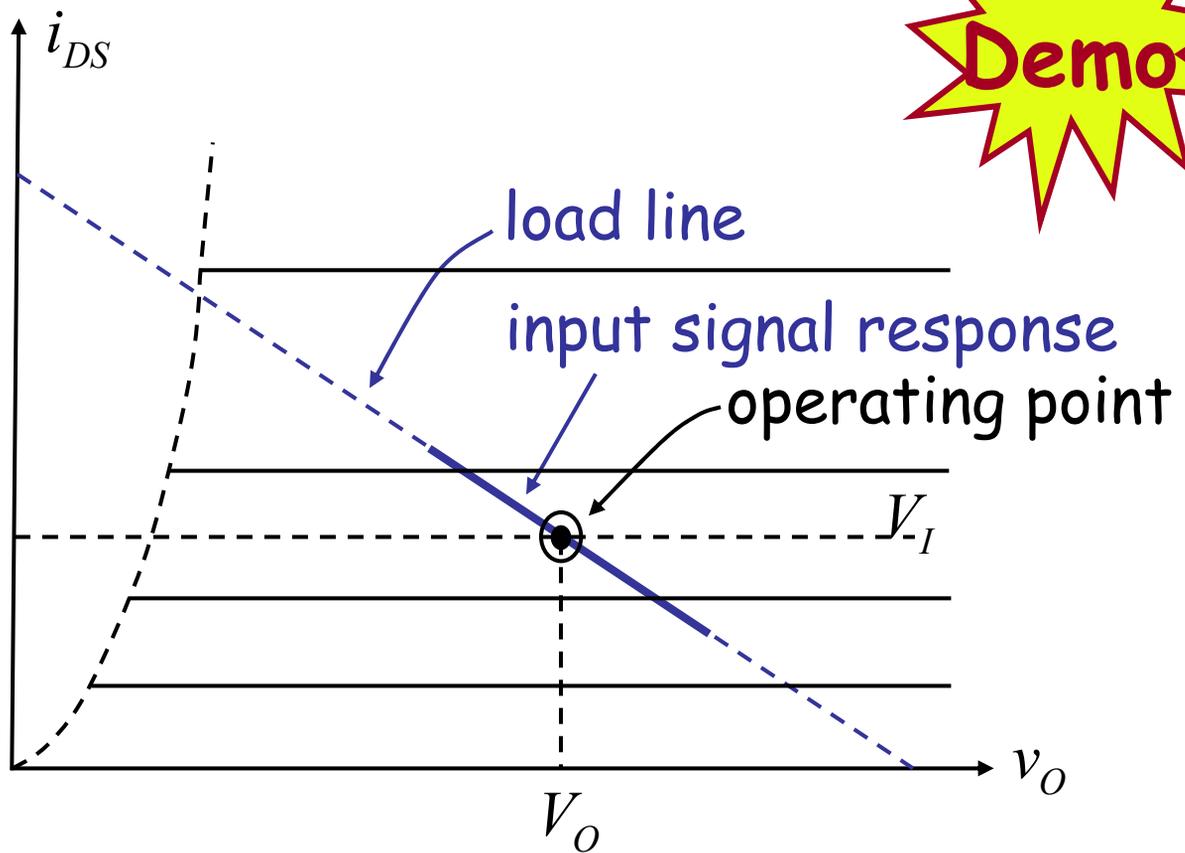
$$v_o = -R_L K (V_I - V_T) \cdot v_i$$

$$g_m = K (V_I - V_T)$$

$$A = -g_m R_L \quad \text{amp gain}$$

Also, see Figure 8.9 in the course notes  
for a graphical interpretation of this result

# More next lecture ...



How to choose the bias point:

1. Gain component  $g_m \propto V_I$
2.  $v_i$  gets big  $\rightarrow$  distortion.  
So bias carefully
3. Input valid operating range.  
Bias at midpoint of input operating range for maximum swing.